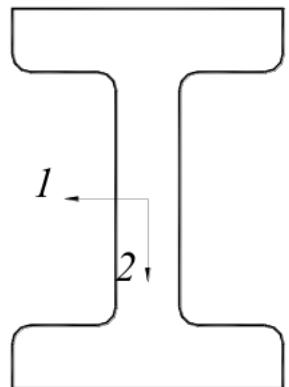
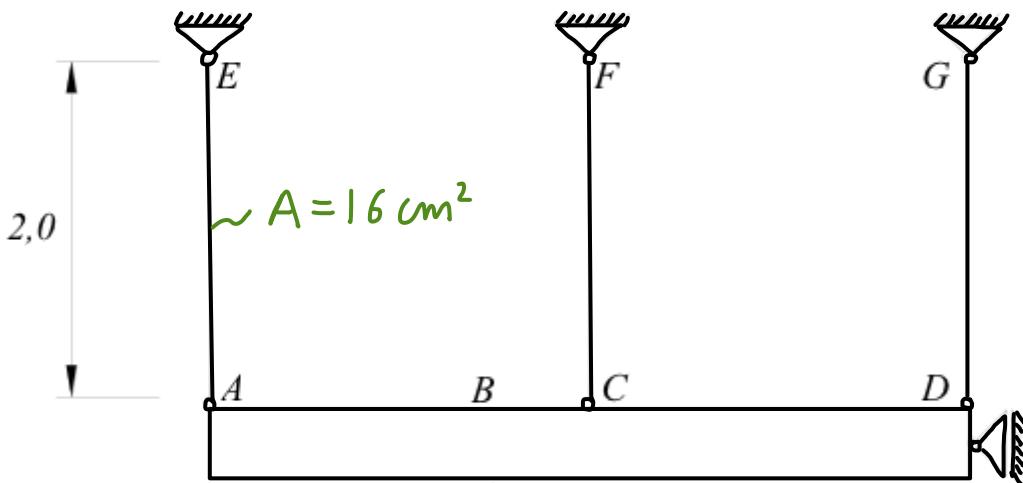


VIGA

IPE300



$$E = 210 \text{ GPa}$$

$$\sigma_c = 235 \text{ N/mm}^2$$

$$I_l = 83,6 \times 10^6 \text{ mm}^4$$

$$Z = 6,021 \times 10^5 \text{ mm}^3$$

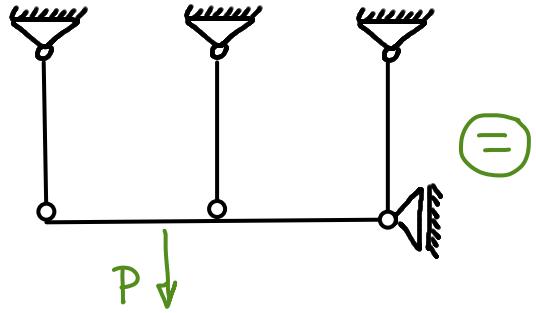
6,284

módulo flexão plástico

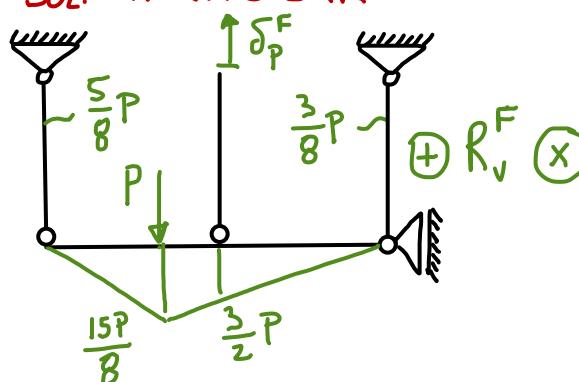
$$N_p = A \bar{\sigma}_c = 376 \text{ kN}$$

$$M_p = Z \bar{\sigma}_c = 147,7 \text{ kNm}$$

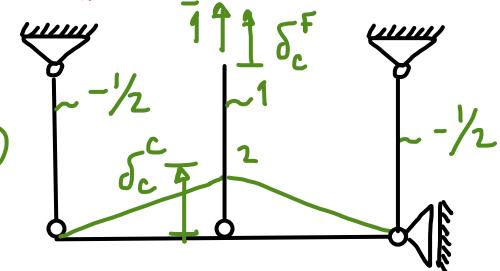
a) diagramas de esforços:



SOL. PARTICULAR



SOL. COMPLEMENTAR



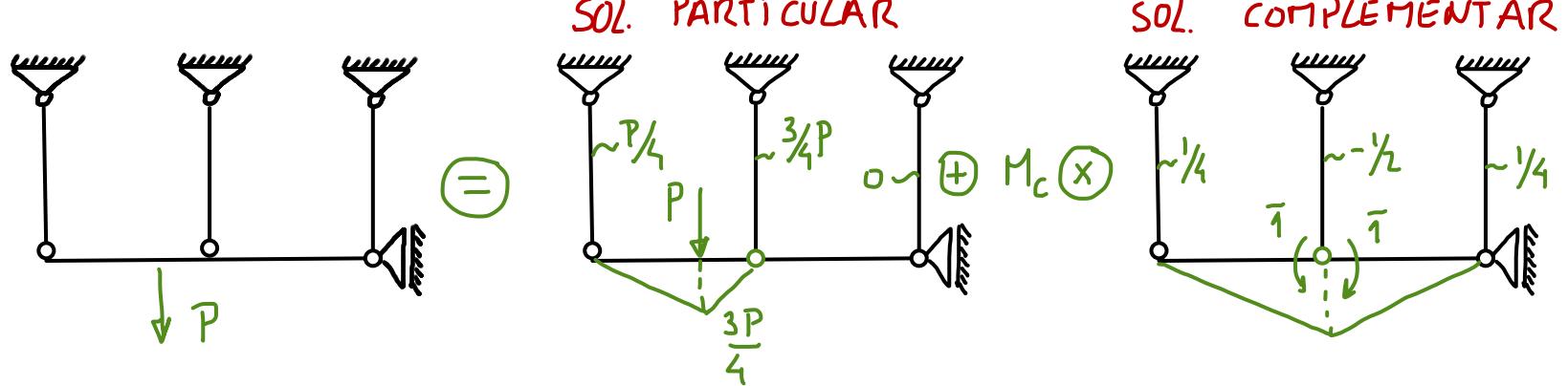
$$\delta_p^F = \frac{1}{EI} \int \left(\frac{5}{8}P \right) \frac{1}{4} dx + \frac{1}{EA} \int \left[-\frac{1}{z} \left(-\frac{5}{8}P + \frac{3}{8}P \right) \right] dx =$$

$$= -\frac{39}{4} \frac{P}{EI} - \frac{P}{EA} = -\frac{P}{E} \left(\frac{39}{4 \times 8356 \times 10^{-8}} + \frac{1}{16 \times 10^{-4}} \right) = -\frac{P}{E} 117,3 \times 10^{-3}$$

$$\delta_c^F = \frac{1}{EI} \int \left(\frac{1}{4} \right)^2 dx + \frac{1}{EA} \left[2 \int \left(\frac{1}{2} \right)^2 dx + \int \left(\frac{1}{2} \right)^2 dx \right] = \frac{32}{3EI} + \frac{3}{EA} = \frac{1}{E} 129,6 \times 10^{-3}$$

$$\delta_p^F + R_v^F \times \delta_c^F = 0 \Rightarrow 129,6 \times 10^{-3} R_v^F = 117,3 \times 10^{-3} \Rightarrow R_v^F = \underline{0,906 P}$$

(SISTEMA BASE ALTERNATIVO)



$$\theta_P^{\text{rel},c} = \frac{1}{EA} \left(\int \left[\frac{P}{2} \right]^{\frac{1}{4}} dx + \int \left[\frac{3P}{4} \right]^{\frac{1}{4}} dx \right) + \frac{1}{EI} \int \begin{array}{c} \text{triangle} \\ \frac{3}{4}P \end{array} dx$$

$$\theta_c^{\text{rel},c} = \frac{1}{EA} \left[2 \int \left(\frac{P}{2} \right)^2 dx + \int \left(\frac{3P}{4} \right)^2 dx \right] + \frac{2}{EI} \int \begin{array}{c} \text{triangle} \\ 1 \end{array} dx$$

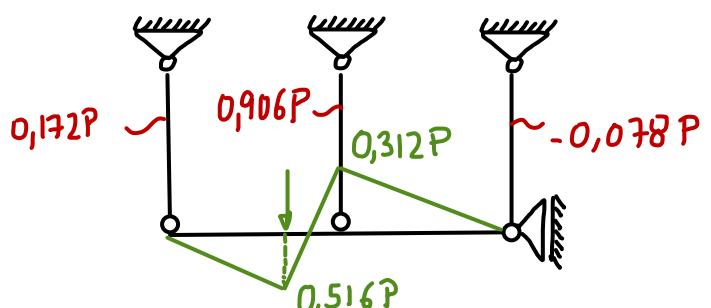
$$\theta_P^{\text{rel},c} + M_c \times \theta_c^{\text{rel},c} = 0 \Rightarrow M_c = -0,312P$$



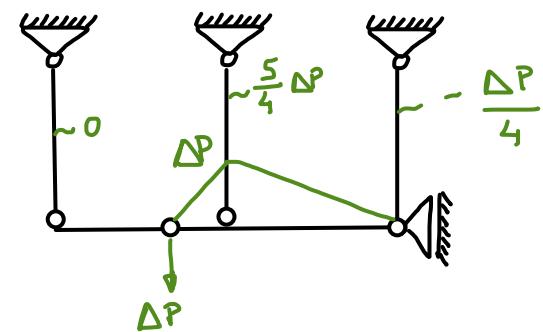
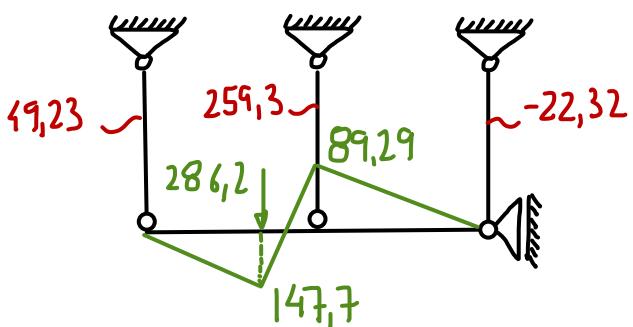
b) determinar carga cedência:

$$0,906P = 376 \Rightarrow P = 415$$

$$0,516P = 17,7 \Rightarrow P = 286,2 \text{ kN} = P_c$$



c1) carga de colapso através de análise incremental:



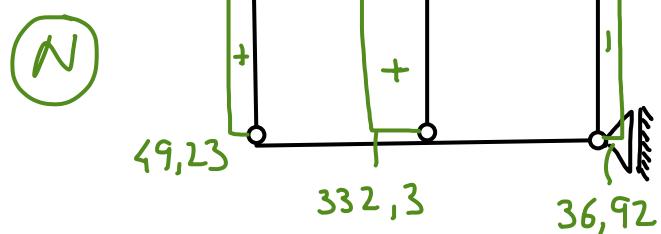
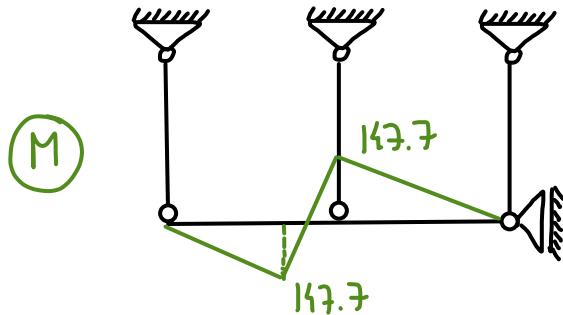
$$259,3 + \frac{5}{4} \Delta P = 376 \Rightarrow \Delta P = 93,36 \text{ kN}$$

$$-22,32 - \frac{\Delta P}{4} = -376 \Rightarrow \Delta P = 1593 \text{ kN}$$

$$89,29 + \Delta P = 147,7 \Rightarrow \Delta P = \underline{\underline{58,41 \text{ kN}}}$$

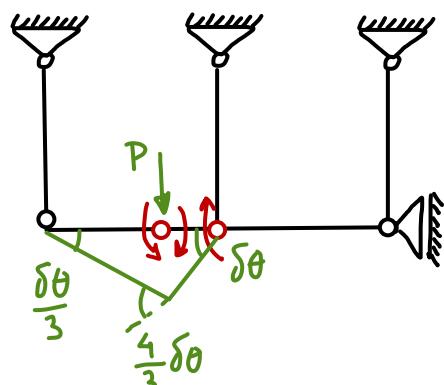
$$\underline{\underline{P_u = P_c + \Delta P = 286,2 + 58,41 = 344,6 \text{ kN}}}$$

d) diagramas de esforços no colapso:



c2) carga de colapso através de análise limite:

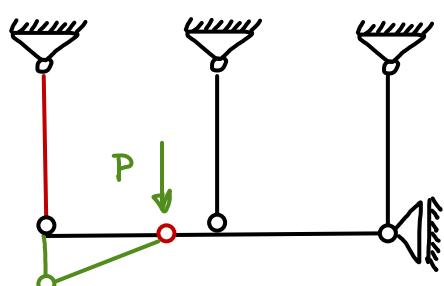
consideram-se apenas mecanismos associados à rotula plástica em B



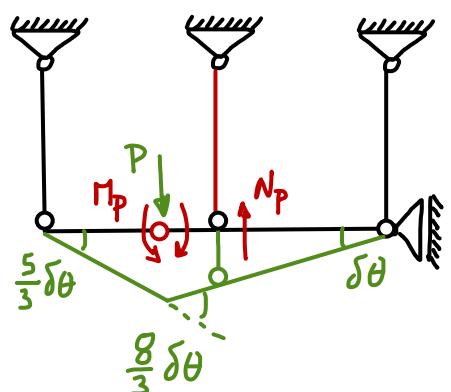
$$\bar{Z}_e = P \delta\theta$$

$$\bar{Z}_D = M_p (\delta\theta + \frac{4}{3} \delta\theta) = M_p \frac{7}{3} \delta\theta$$

$$\bar{Z}_e \geq \bar{Z}_D \Rightarrow P \geq \frac{7}{3} \times 147,7 = \underline{\underline{344,6 \text{ kN}}}$$



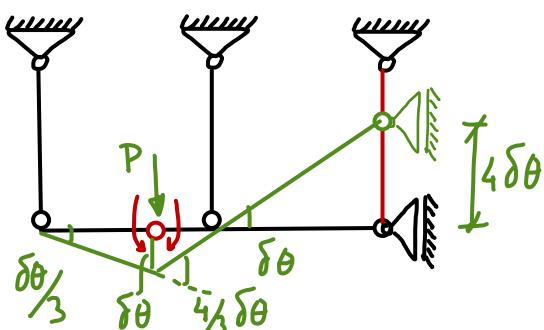
$$\bar{Z}_e = 0 \Rightarrow \text{mecanismo impossível}$$



$$\bar{Z}_e = 5 \delta\theta P$$

$$\begin{aligned} \bar{Z}_D &= \left(\frac{8}{3} M_p + 4 N_p \right) \delta\theta = \left(\frac{8}{3} 147,7 + 4 \times 37,6 \right) \delta\theta \\ &= 1898 \delta\theta \end{aligned}$$

$$\bar{Z}_e \geq \bar{Z}_D \Rightarrow P \geq 379,6 \text{ kN}$$



$$\bar{Z}_e = P \delta\theta$$

$$\bar{Z}_D = M_p (\delta\theta + \frac{\delta\theta}{3}) + 4 N_p \delta\theta = 1701 \delta\theta$$

$$\bar{Z}_e \geq \bar{Z}_D \Rightarrow P \geq 1701 \text{ kN}$$