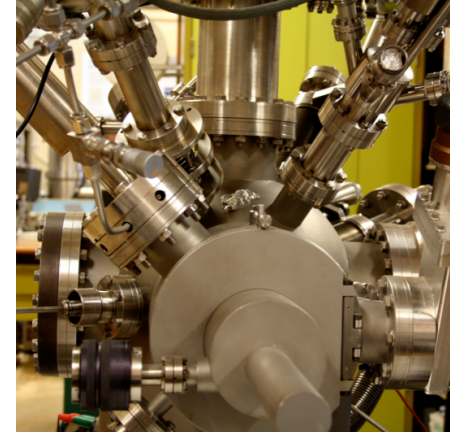
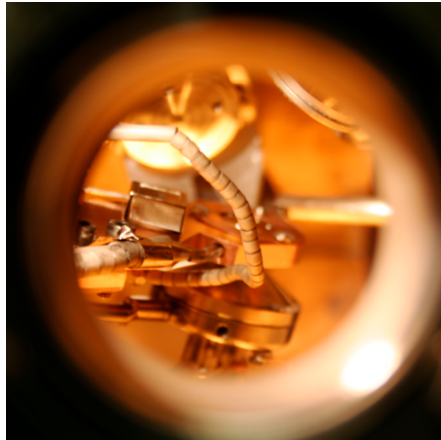




FACULDADE DE  
CIÊNCIAS E TECNOLOGIA  
UNIVERSIDADE NOVA DE LISBOA



# Calibration of reference leaks in a wide pressure range

Ana L. Fonseca, A. Marta Barreto, A. Sofia Matos, A.M.C.Moutinho  
and [Orlando M.N.D.Teodoro](#)

# + Outline

- Motivation
  - Reference leaks for sniffers, R134a leaks
- Calibration set-up
  - Syringe and stepper motor
  - User interface
  - Measuring range
  - Temperature effects
  - Repeatability
  - Time needed for calibration
- Typical uncertainty
- Method validation
- Typical results
  - R134a and He leaks

## + Motivation: reference leaks for sniffers

- Inside-out He leak detection technique (sniffer)
  - He reference leaks in the range  $10^{-6}$  to  $10^{-5}$  mbar.L/s
- 842/2006 regulation and subsequent statements
  - R134a reference leaks of 5 g/year



REGULATION (EC) No 842/2006 OF THE EUROPEAN PARLIAMENT AND OF THE COUNCIL  
of 17 May 2006  
on certain fluorinated greenhouse gases

COMMISSION REGULATION (EC) No 1516/2007  
of 19 December 2007

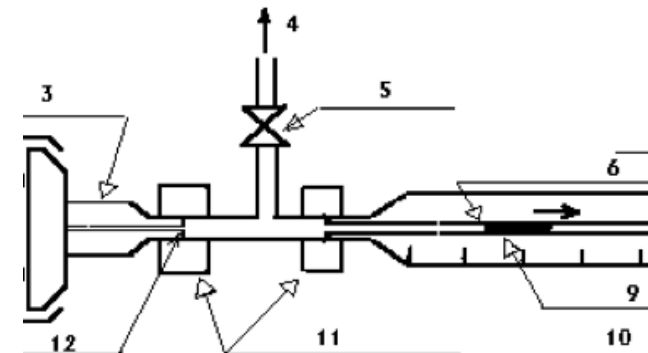
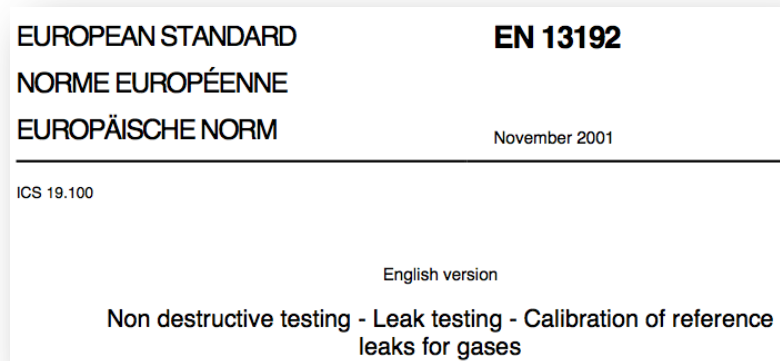
establishing, pursuant to Regulation (EC) No 842/2006 of the European Parliament and of the Council, standard leakage checking requirements for stationary refrigeration, air conditioning and heat pump equipment containing certain fluorinated greenhouse gases

2. Gas detection devices referred to in paragraph 1(a) shall be checked every 12 months to ensure their proper functioning. The sensitivity of portable gas detection devices shall be at least five grams per year.



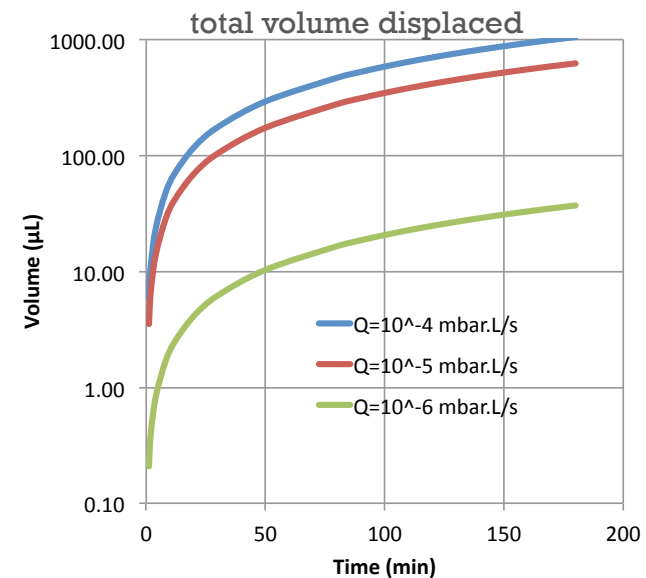
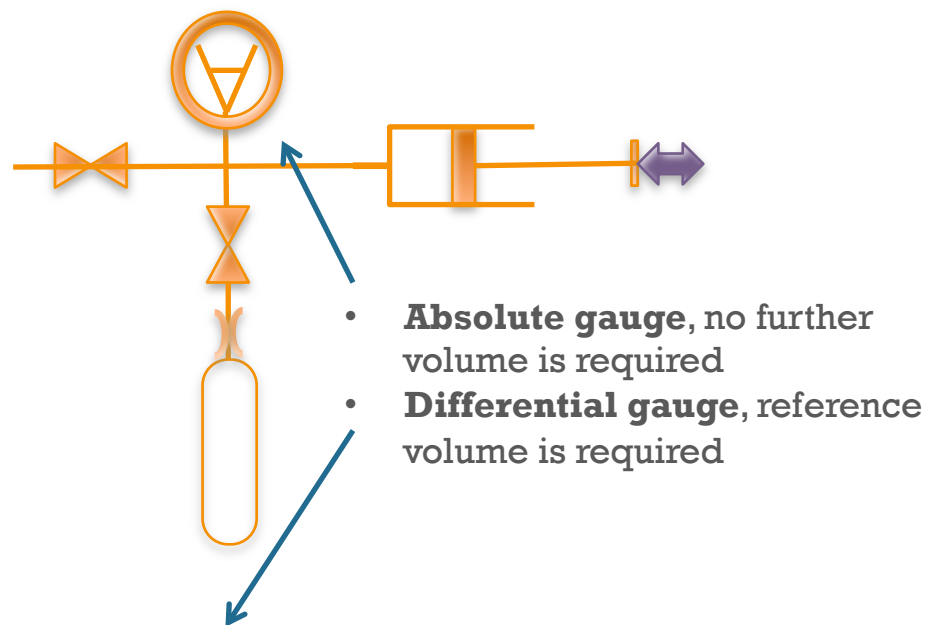
## + Motivation

- Calibration by comparison using a MS leak detector is not suitable
  - Calibration pressure should be atmosphere, not vacuum
- EN 13192 method C: calibration of leaks from overpressure to atmosphere
  - Capillary with a moving slug
  - Although very simple, is of limited application (slug friction, pressure control, etc.)
- However,  $p\Delta V$  method is well suited



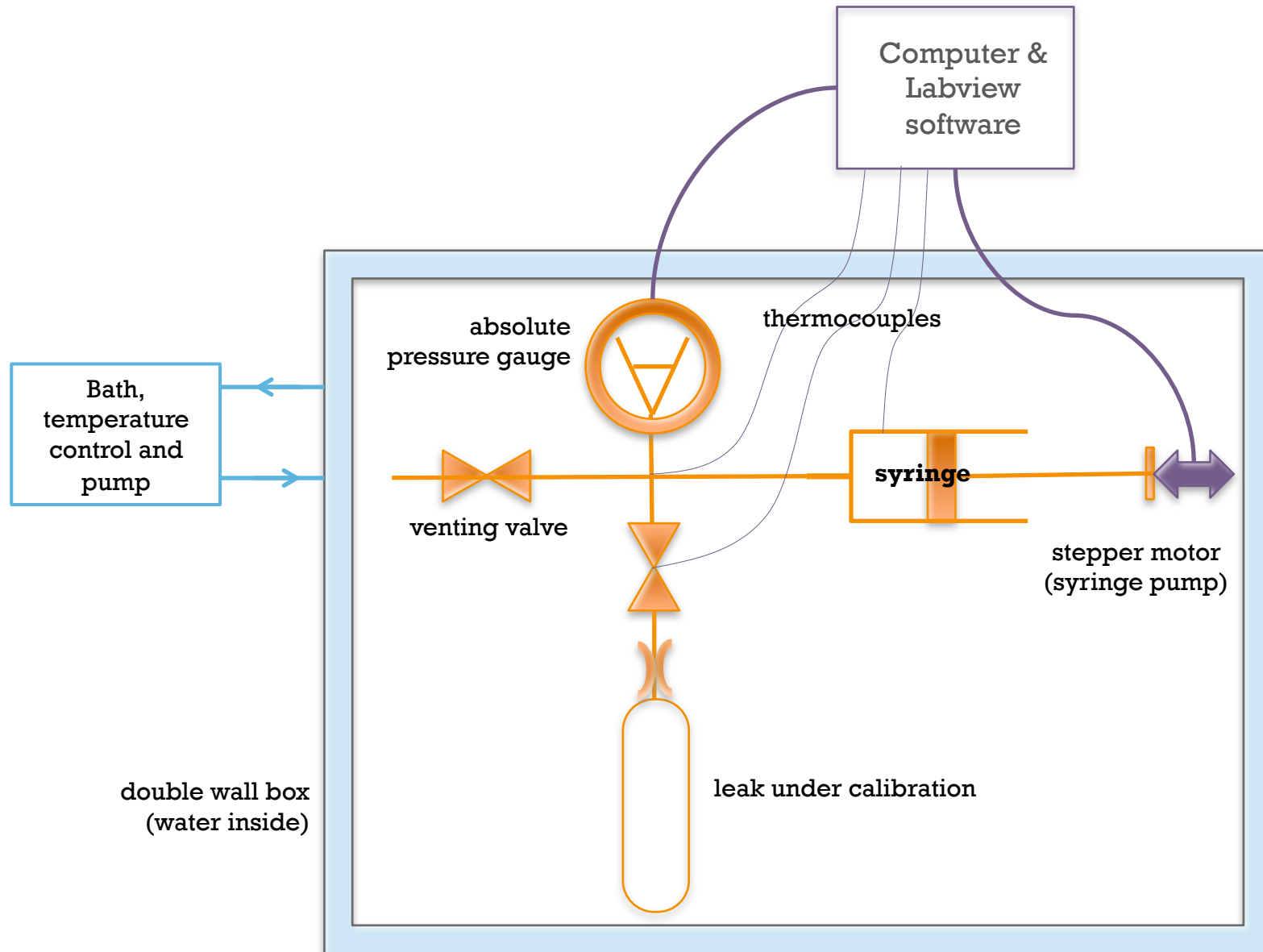
## + Calibration method: $p\Delta V$

- The leak is connected to a closed volume
- A piston is actuated every time a pressure increase is detected to keep the pressure constant
  - Volume  $\approx 1$  mL, step  $< 1\ \mu\text{L}$  (resolution)



1. M. Bergoglio e D. Mari, "INRIM primary standard for microgas-flow measurements with reference to atmospheric pressure" *Measurement* 45 (2012) 2459
2. K. Jousten e U. Becker, "A primary standard for the calibration of sniffer test leak devices," *Metrologia*, 46 (2009) 560-568
3. F. Boineau, "Characterization of the LNE constant pressure flowmeter for the leak flow rates measurements with reference to vacuum and atmospheric pressure," *PTB-Mitteilungen*, 121 (2011) 313

# + Calibration set-up



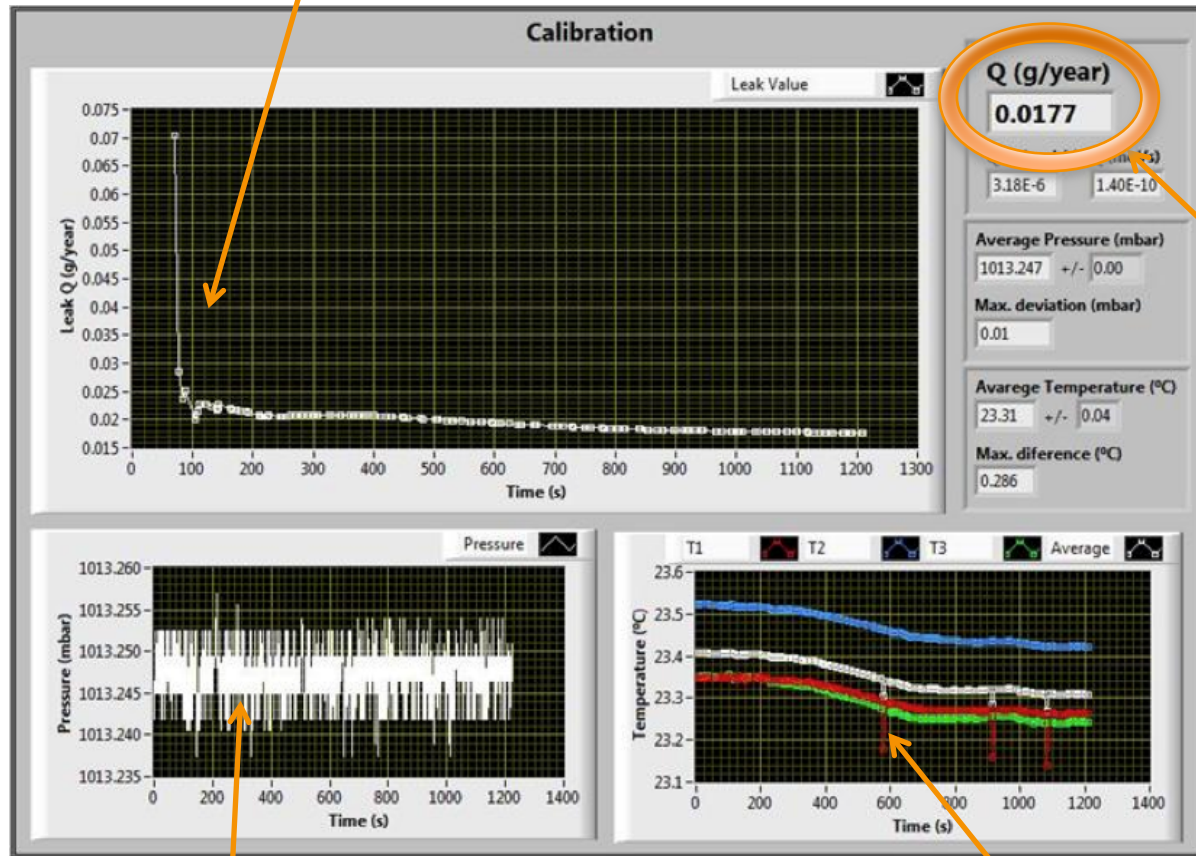
## + Calibration set-up

- Piston: **1 mL** SGE gas tight syringe with PTFE plunger tip
- Piston actuator: syringe pump NE-500
  - 800 steps/revolution; 1 step  $\approx$  1.7  $\mu$ m
- Gauge: Druck DPI 142 precision Barometer
  - Resolution  $\approx 3 \times 10^{-3}$  mbar; piezo sensor
- Software: Labview platform
- Tubing: 1/8" swagelok fittings and valves
- Stainless steel double wall box with 2 computer fans inside to increase temperature homogeneity
- Water circulator Julabo F25-ED



# + User interface

Flow rate (integrated measurement), converges with time



Actual measurement

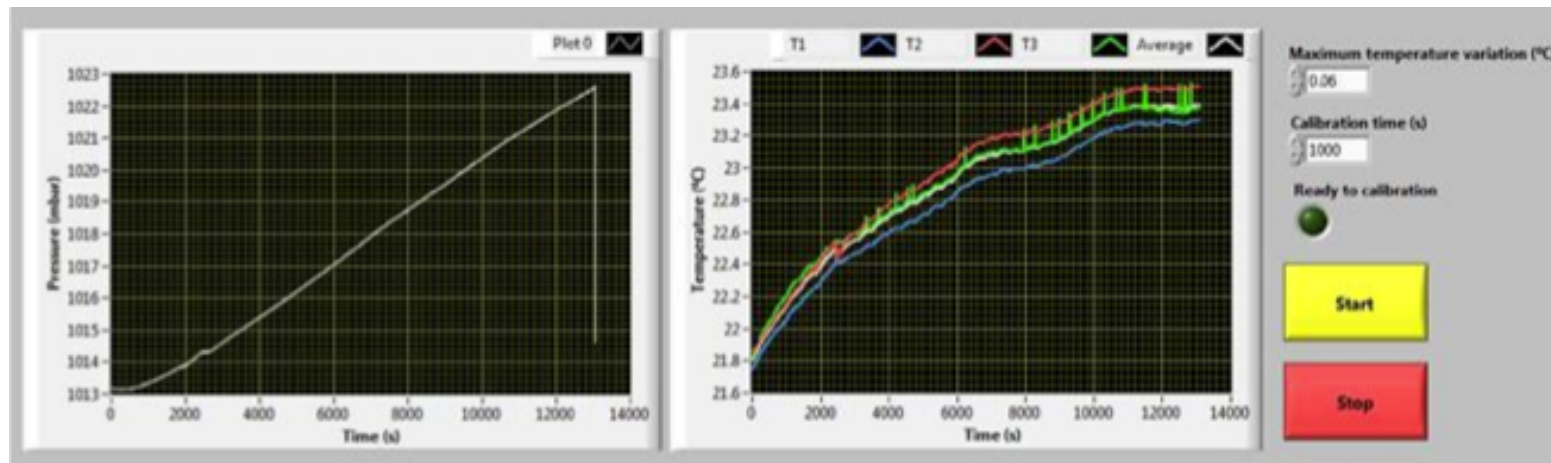
Pressure ( $\approx 10^{-2}$  mbar maximum variation)

Temperature drift (3 thermocouples), critical to achieve low uncertainty



## + Before calibration

- $\Delta pV$  method, for preliminary evaluation
- temperature stability confirmation



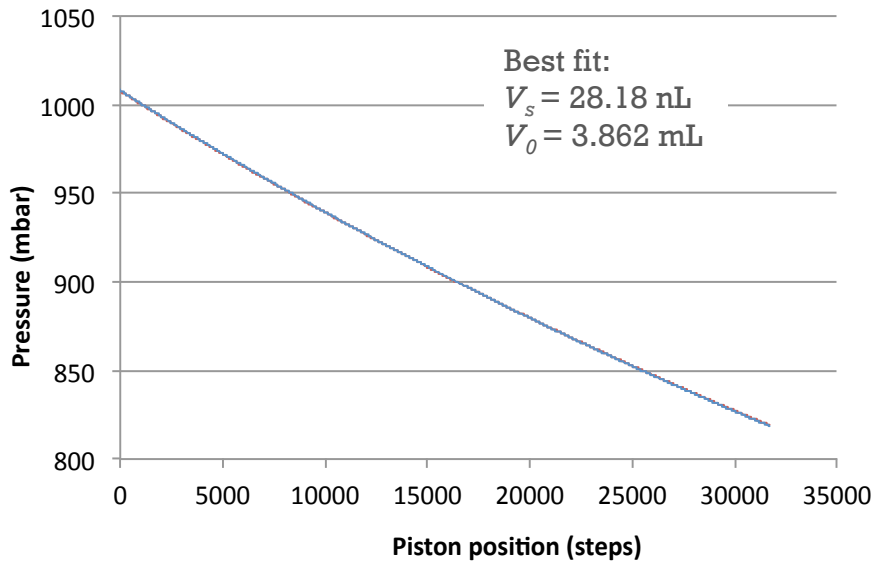
# + Syringe characterization

- Gravimetric volume calibration
  - Step volume  $V_s = 28.0 \pm 0.22$  nL
- Syringe expansion without leak
  - Boyle-Mariotte relation
  - Full volume range  $\approx 32\ 000$  steps
- Step volume  $V_s$  and dead volume  $V_0$  can be calculated by fitting these parameters in the experimental data

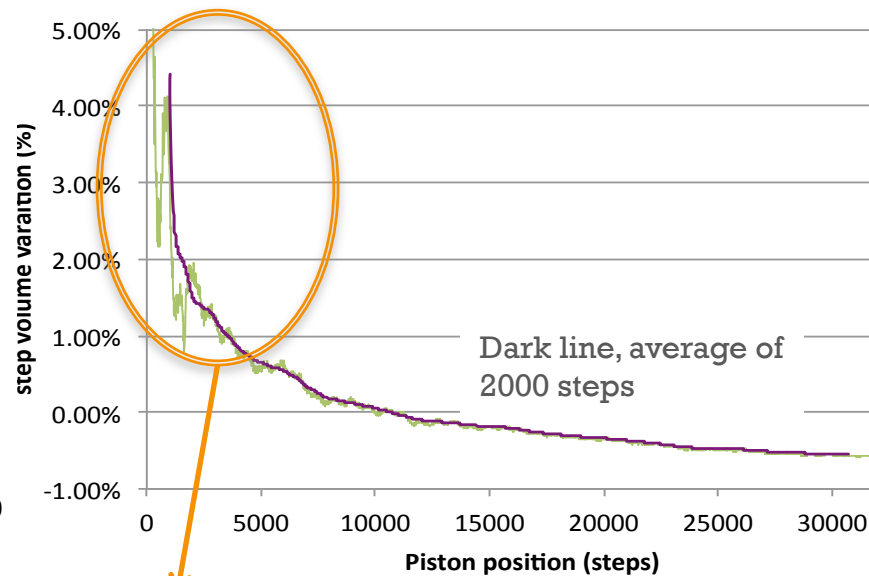
$$p = \frac{p_0 V_0}{nV_s + V_0}$$

fitting parameters

$$V_s = \frac{V_0}{n} \left( \frac{p_0}{p} - 1 \right)$$



Step volume as function of position



most used position = larger diameter

## + Measuring range, time needed for calibration

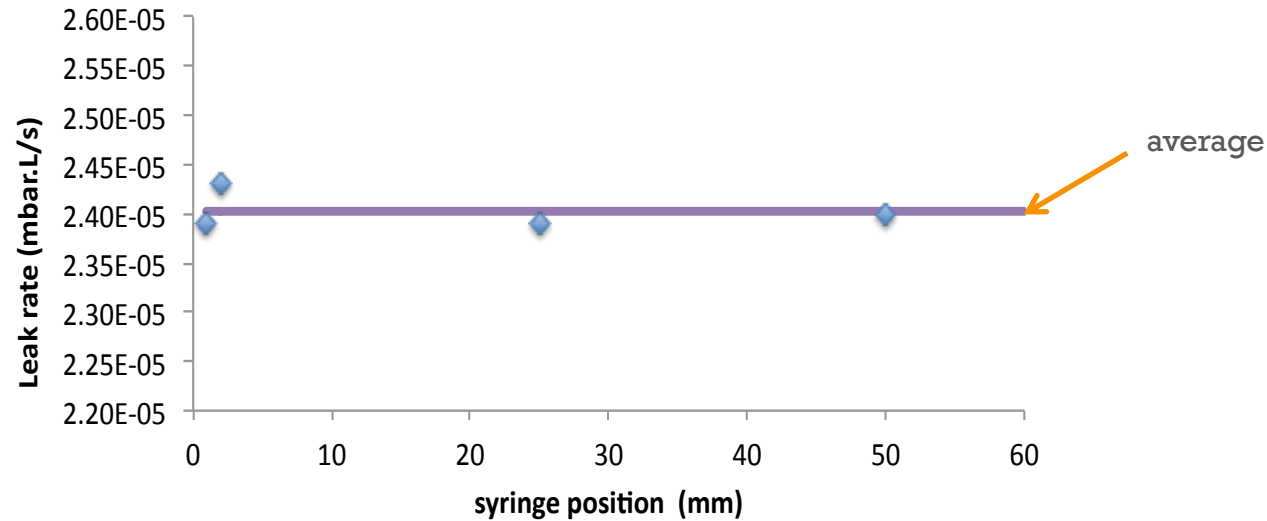
- 2000 steps averages thread defects

total steps	Q	time		
		s	min	h
2000	$10^{-4}$ mbar.L/s	560	9.3	
	$10^{-5}$ mbar.L/s	5600	93.3	1.6
	$10^{-6}$ mbar.L/s	56000	933.3	15.6
	5 g/year R134 a	1474	24.6	

## + Repeatability

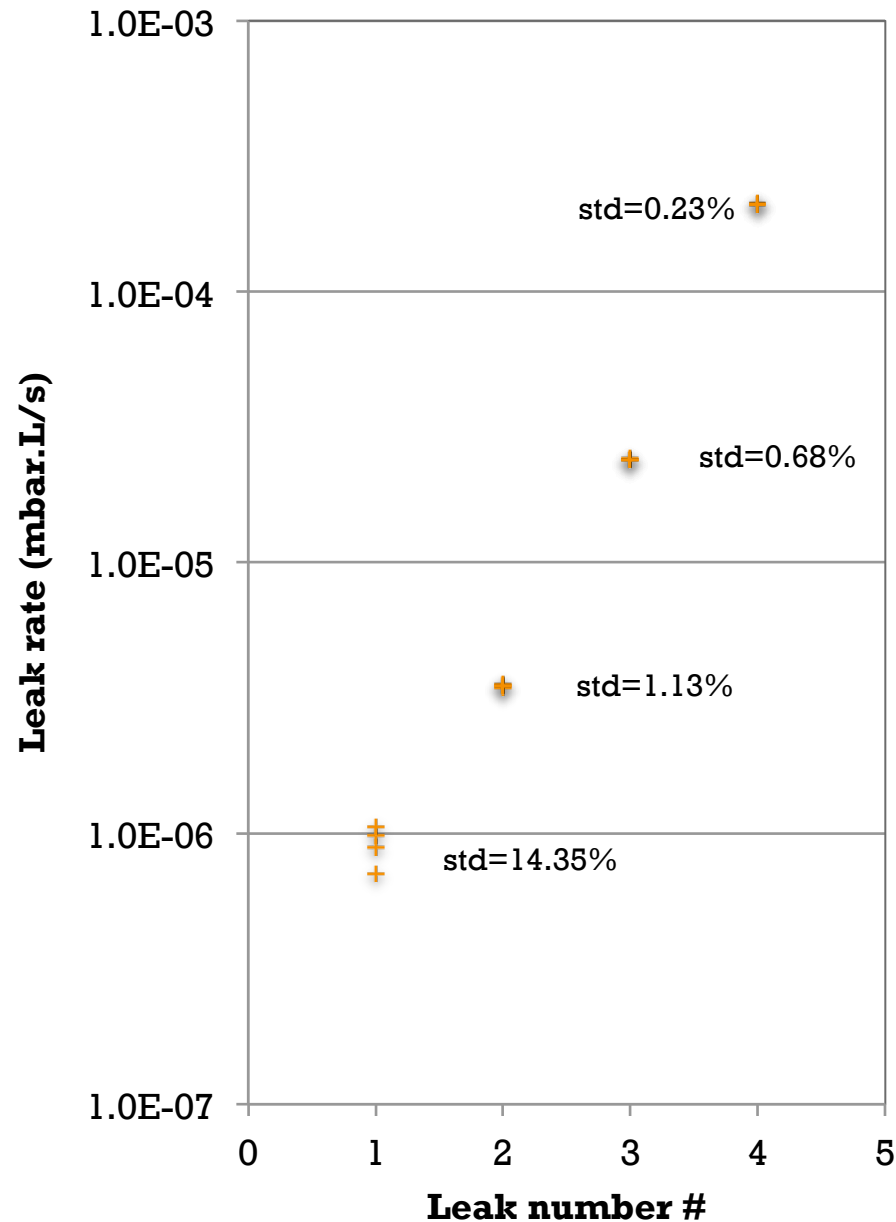
### ■ Effect of the position of the syringe plunger tip (piston)

He leak, nominal leak rate =  $2.60 \times 10^{-5}$  mbar.L/s calibrated to vacuum



## + Repeatability

- 4 different leaks were measured 4 times each
- Repeatability depends on:
  1. Number of steps (acquisition time)
  2. Temperature drift has a major impact
  3. Leak stability
- On the graph 1000 to 10000 steps were used.



## + Typical uncertainty

- R134a leak,  $Q=3.48$  g/year

Quantity, $x_i$	Estimate	$u(x_i)$	$c_i u(x_i)/d$ (g/year)	relative contribution %
pressure	1000 mbar	0.015 mbar	1.54E-05	0.027
volume	22 $\mu$ L	0.17 $\mu$ L	7.79E-03	13.7
temperature	296.9 K	0.06 K	5.38E-04	0.4
time	827 s	$9.6 \times 10^{-3}$ s	1.16E-05	0.02
repeatability ( $\Delta T \approx 0.1$ K)		0.17 g/year	0.049	85.9
<b>Total (k=2)</b>			<b>0.098</b> <b>2.82%</b>	100

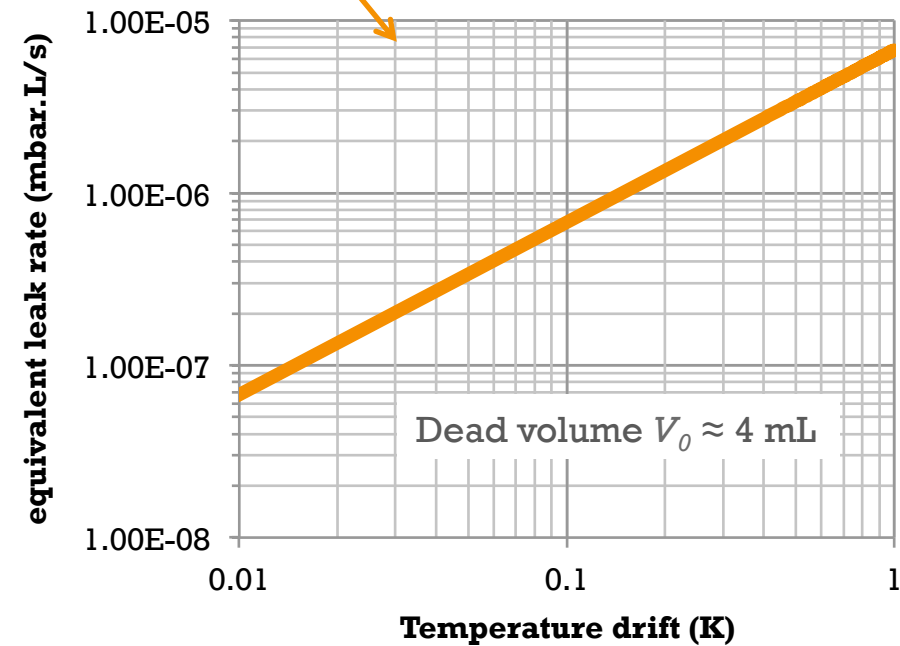
$$Q = 3.48 \pm 0.10 \text{ g/year}$$

## + Temperature effects

- The use of an absolute gauge turns this calibration set-up more sensitive to temperature drifts
  - A drift in the temperature is equivalent to a **temporary virtual leak** (positive or negative)
  - This effect is slightly cancelled by tubing dilatation

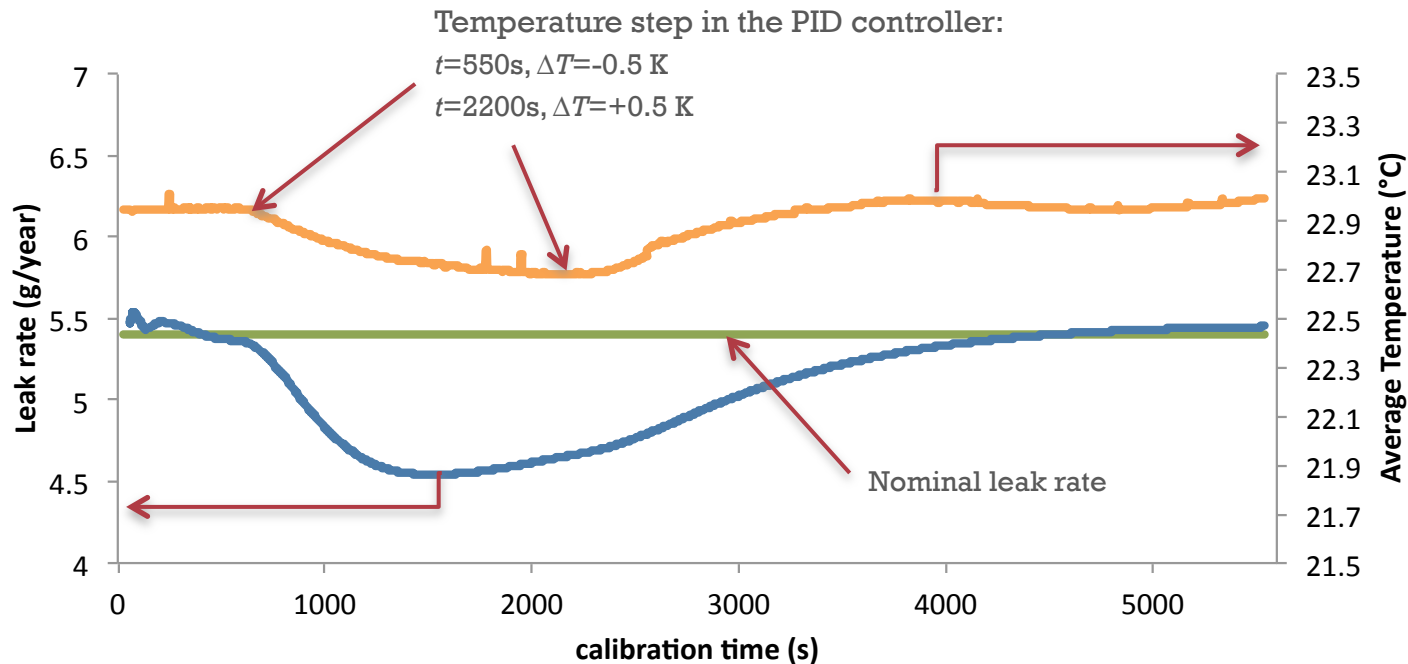
Gay-Lussac law

$$Q_{eq} = \frac{p_0 V_0}{t} \left( \frac{T_0 + \Delta T}{T_0} - 1 \right)$$



## + Temperature effects

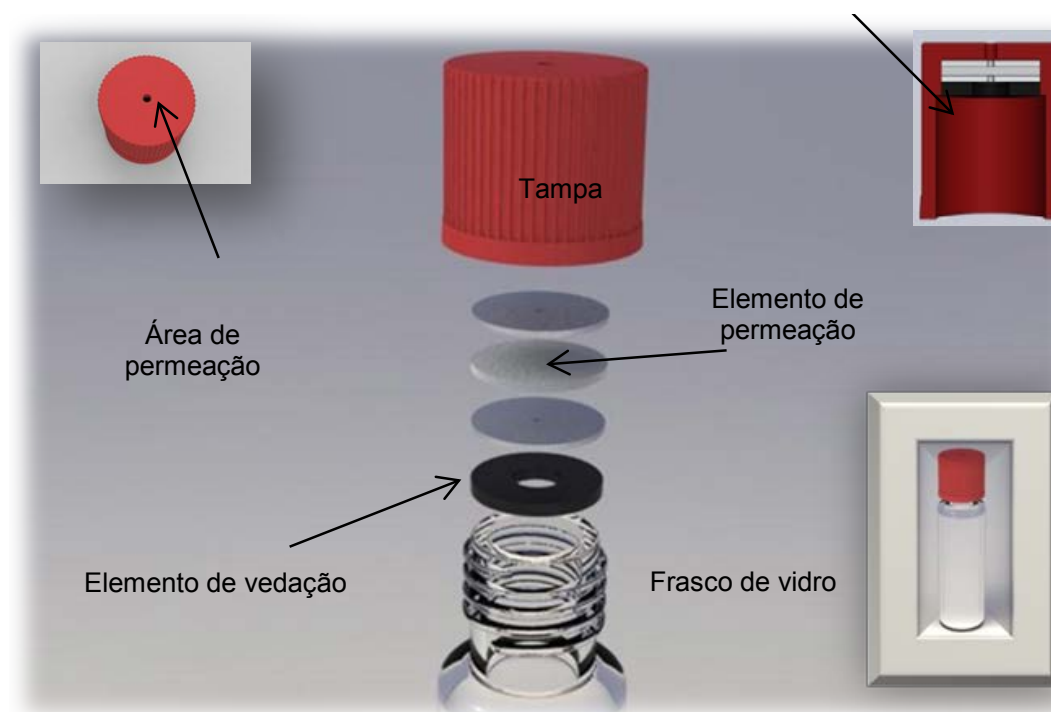
- Total temperature drift is more important than temperature uniformity.
  - If temperature changes slowly, what matters is the difference between the starting temperature and the final temperature
- Experiment: induced temperature step
  - Temperature effects may be cancelled by positive and negative drifts





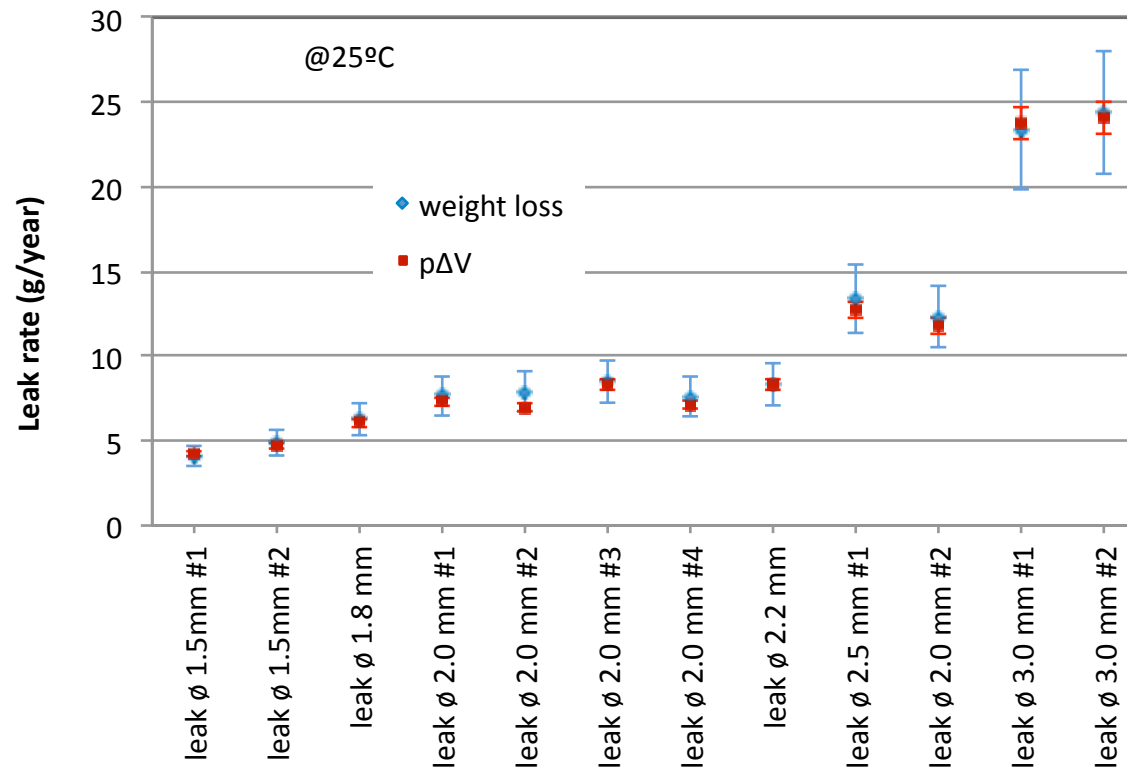
## + Method validation

- A series of R134a leaks were built with leak rates ranging 4 to 24 g/year



## + Method validation

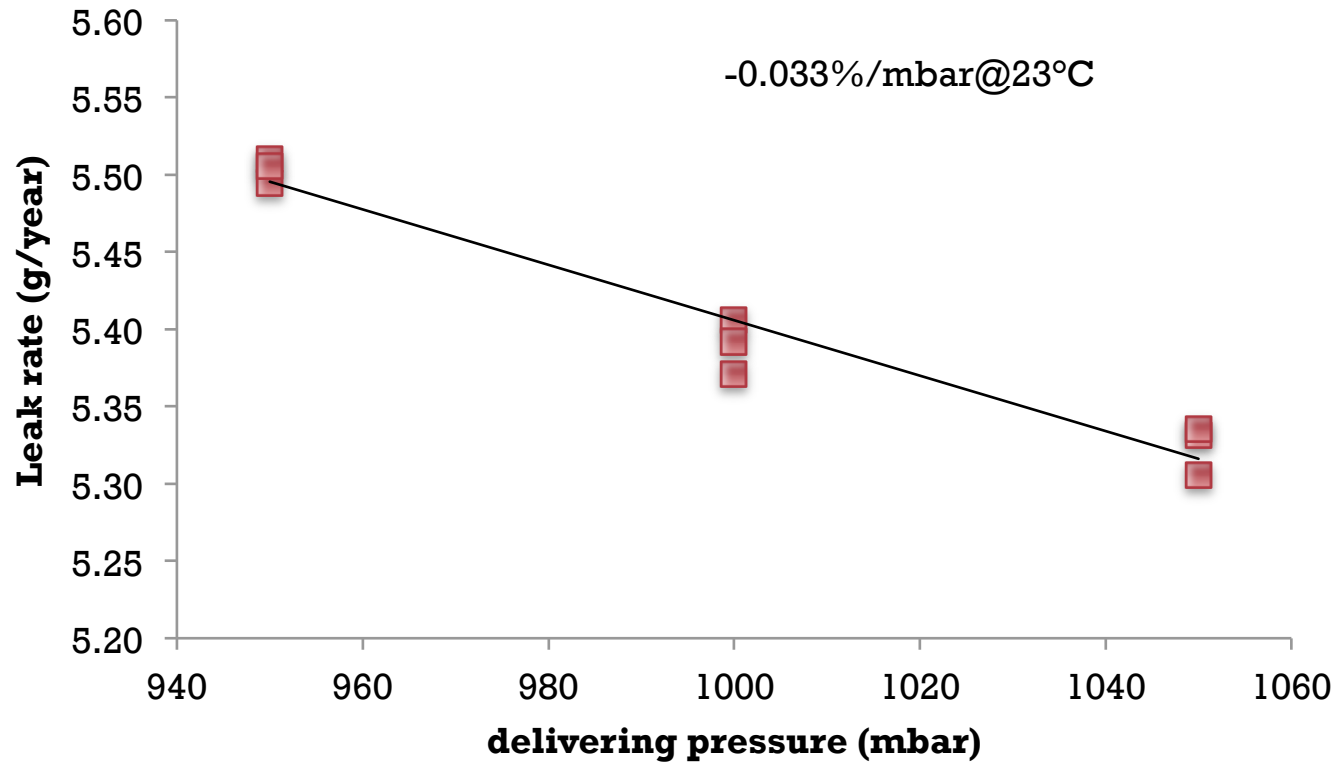
- Leaks were weighted over several days ( $U=\pm 15\%$ ) and leak rate calculated.
- Then, all leaks were calibrated in the  $p\Delta V$  set-up and compared



## + R134a reference leaks

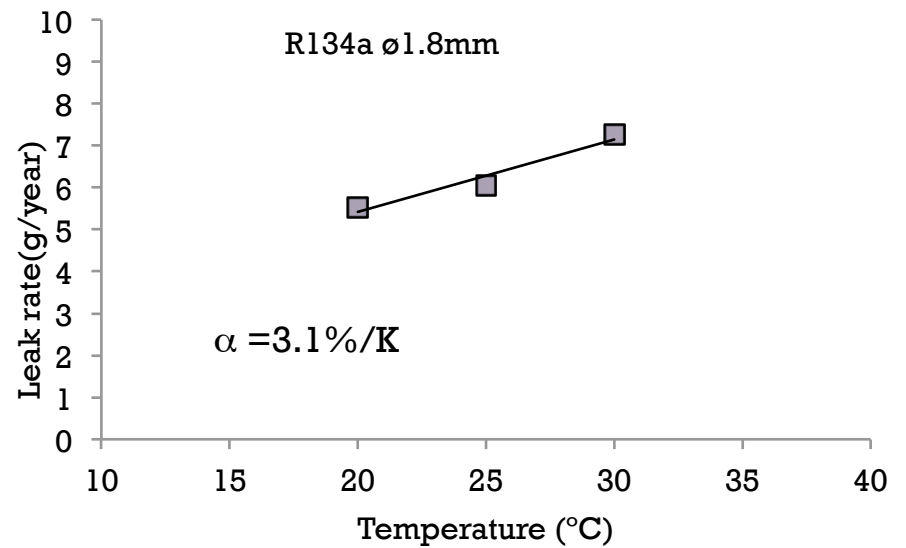
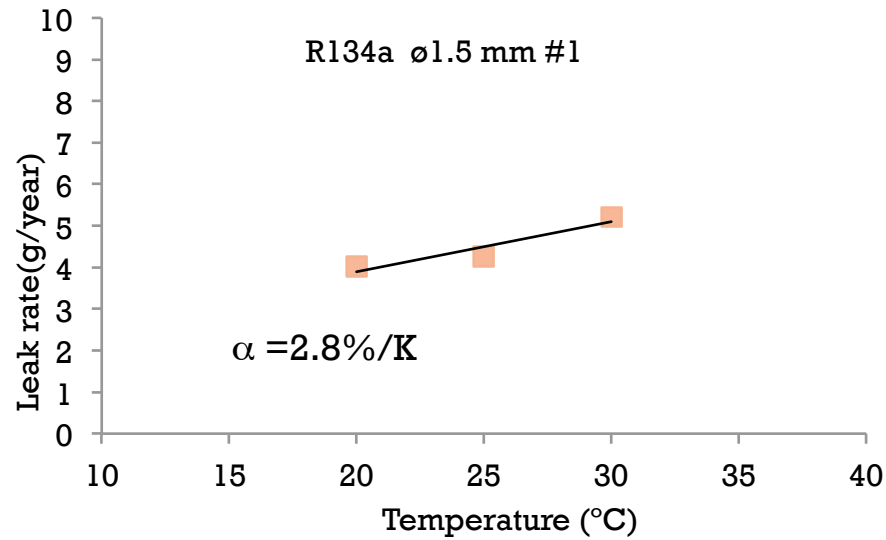
- Dependence on the delivering pressure
  - 2000 steps measurements  $\approx$  25 min

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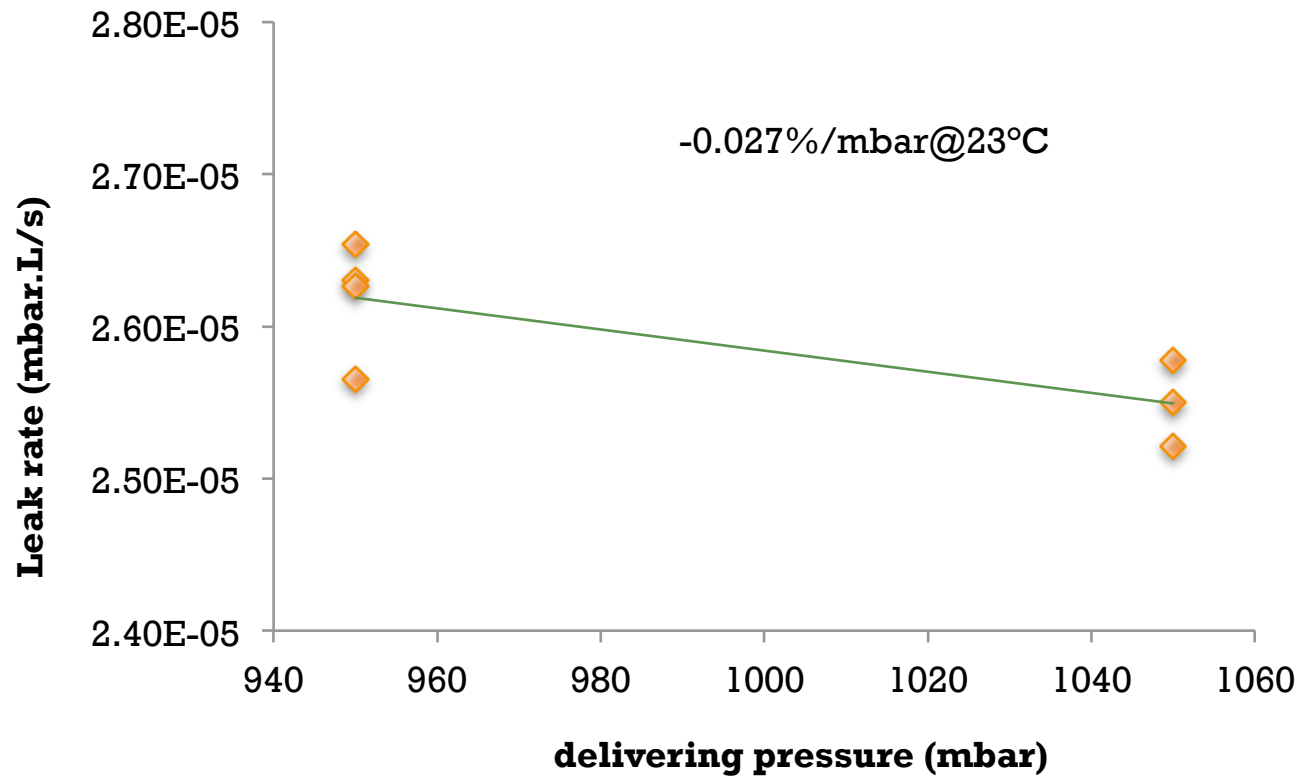
# + R134a reference leaks

- Dependence on the temperature



## + He reference leaks (permeation)

- Dependence on the delivering pressure
  - 2000 steps measurements  $\approx$  35 min



## + Conclusions

- $p\Delta V$  calibration method was assembled with a syringe pump and is properly working at Metrovac laboratory in Lisbon.
- One absolute pressure gauge is used
  - This gauge is suitable to measure both the calibration pressure and the pressure change
- Temperature stability is critical to achieve good uncertainty
- Uncertainties  $\approx 3\%$  are easily achieved for the range of  $10^{-5}$  mbar.L/s or 5g/year
- R134a reference leaks were developed and fully characterized.
  - These leaks were used to validate the method



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*Thanks for your attention*

odt@fct.unl.pt